

Corrosion.m, a *Mathematica*<sup>TM</sup> PACKAGE for  
doing ELECTROCHEMISTRY and CORROSION  
by COMPUTER

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*Mathematica*<sup>TM</sup> is a general system for doing numerical and symbolics calculations or two and three-dimensional graphics, as well as a programming language and a computing environment<sup>1</sup>. Corrosion.m is a package designed for electrochemistry and corrosion studies in the field of research and education. Corrosion.m is available upon request by e.mail at [erase@grenet.fr](mailto:erase@grenet.fr). Two examples of use are presented below.

### Validity of the Tafel slope extrapolation method

Built-in Mathematica graphics functions such as Plot are useful for drawing and studying the influence of parameters upon the shapes of the polarization curves and limitations of the so-called Tafel slope extrapolation method (fig. 1)<sup>2,3,4</sup>. Corrosion.m includes, for this purpose, Butler-Volmer equations. Figure 1 shows the Tafel slope extrapolation method for a corroding metal when the corrosion potential lies close to the reversible potential of the metal. The corrosion density current error can be estimated for equal Tafel slopes ( $b_{a1} = b_{a2} = b_a$ ,  $b_{c1} = b_{c2} = b_c$ ) in the absence of transport limitations. In this restricted case the corrosion current  $i_{\text{corTafel}}$  measured by Tafel slope extrapolation method is given by

$$\begin{aligned} i_{\text{corTafel}} &= i_{01} \exp [2.3 (E_c - E_{\text{th1}})/b_a] + i_{02} \exp [2.3 (E_c - E_{\text{th2}})/b_a] \\ &= i_{01} \exp [-2.3 (E_c - E_{\text{th1}})/b_c] + i_{02} \exp [-2.3 (E_c - E_{\text{th2}})/b_c] \end{aligned} \quad (1)$$

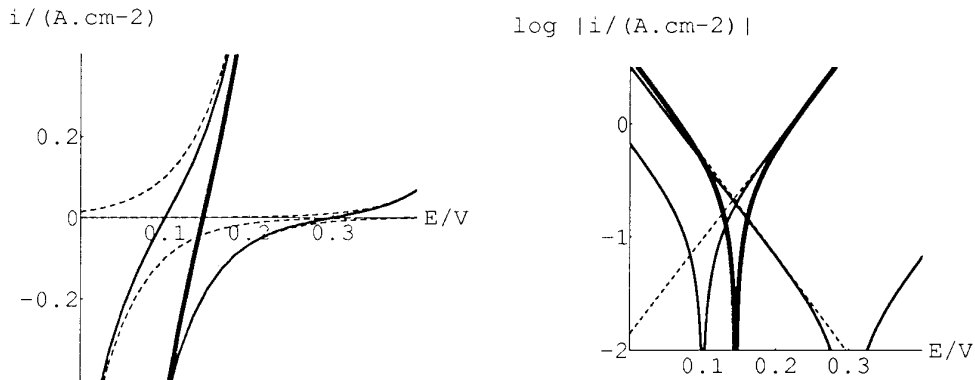
<sup>1</sup> S. Wolfram, *Mathematica*<sup>TM</sup>, Addison Wesley, Redwood City (1988).

<sup>2</sup> F. Mansfeld, The polarization resistance technique for measuring corrosion currents, *Advances in Corrosion and Technology*, Vol. 6, Ed. M. G. Fontana and R. W. Staehle, Plenum Press, New York, 1976.

<sup>3</sup> D. Landolt, *Corrosion et chimie des surfaces des métaux*, Presses Polytechniques et Universitaires Romandes, Lausanne, 1993.

<sup>4</sup> J.-P. Diard, B. Le Gorrec, C. Montella, *Cinétique Electrochimique*, to be published.

where  $i_{01}$  and  $i_{02}$  are the exchange density currents,  $E_{th1}$  and  $E_{th2}$  the reversible potentials, and  $E_c$  is the corrosion potential. The true corrosion current  $i_{cor}$  is given by



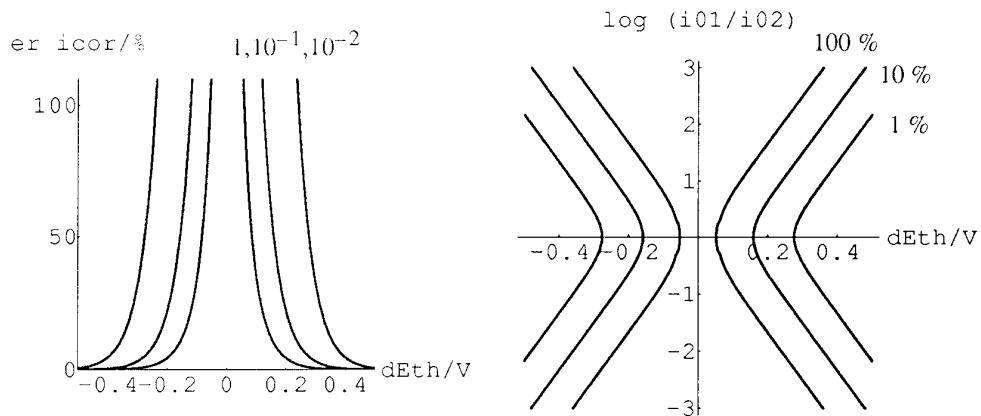
**Figure 1 :** Theoretical polarization curves for a corroding metal when the corrosion potential lies close to the reversible potential of the metal. Thick and thin lines : overall current, dashed lines : partial currents ( $i$  vs  $E$  curve) or Tafel lines.  $E_{th1} = 0.1$  V,  $E_{th2} = 0.3$  V,  $i_{01} = 10^{-1}$  A.cm $^{-2}$ ,  $i_{02} = 10^{-2}$  A.cm $^{-2}$ ,  $b_{a1} = b_{c1} = b_{a2} = b_{c2} = 0.12$  V.

$$i_{cor} = i_{01} (\exp [2.3 (E_c - E_{th1})/b_{a1}] - \exp [2.3 (E_c - E_{th1})/b_{c1}]) \quad (2)$$

The relative error can be expressed as<sup>5</sup>

$$er i_{cor} = 100 (i_{corTafel} - i_{cor})/i_{cor} \quad (3)$$

For the example in Fig. 2 the above error is equal to  $\approx 20$  %. The corrosion potential is numerically calculable with the FindRoot function allowing to plot the isoerror diagram using the ContourPlot function (Fig. 2).



**Figure 2 :** Plot of  $er i_{cor}$  against  $dE_{th} = E_{th1} - E_{th2}$  calculated for  $i_{01}/i_{02} = 1, 10^{-1}, 10^{-2}$  and isoerror diagram.  $b_a = b_c = 0.12$  V. The contours correspond to errors of 1 %, 10 % and 100 %.

<sup>5</sup> Z. Nagy, DC Electrochemical techniques for the measurement of corrosion rates, Modern Aspect of Electrochemistry, N $^{\circ}$  25, edited by J. O'M Bockris et al. Plenum Press, New York, 1993.

### Corrosion current measurements by curve fitting

Mathematica's numerical functions as NonlinearFit can be used to design new measuring method in the field of corrosion studies.

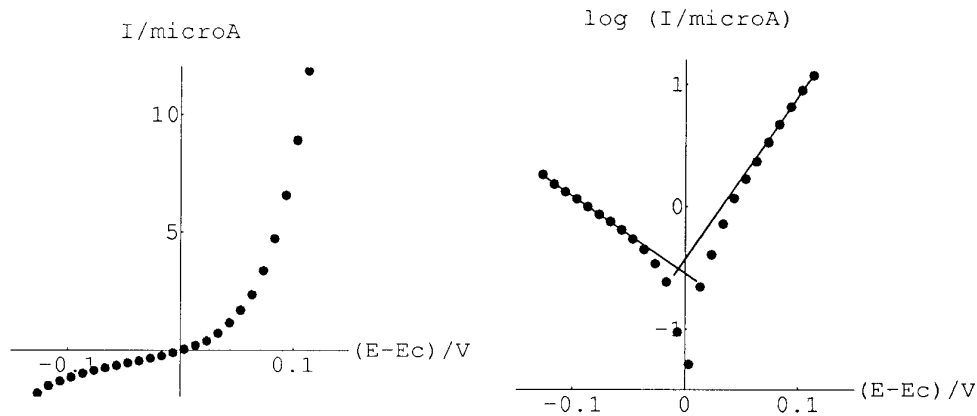


Figure 3 : Experimental data and Tafel slope extrapolation method (4 anodic experimental points and 7 cathodic one). Rotating disk electrode : Fe (Johnson Matthey 99.9985 %) in deaerated acidic medium (HCl 0.1 M, KCl 0.9 M),  $S = 7.85 \cdot 10^{-3} \text{ cm}^2$ ,  $\Omega = 10^3 \text{ rpm}$ .  $I_{\text{cor}} = 0.31 \text{ } \mu\text{A}$ ,  $b_a = 0.075 \text{ V}$ ,  $b_c = 0.16 \text{ V}$ .

As an example the current vs potential curve for a Fe rotating disk electrode in an acidic medium is shown in the figure 3. The measurements were carried out within a narrow range of potential ( $\approx 0.25 \text{ V}$ ). It is nevertheless possible to determine the corrosion current by Tafel slope extrapolation (Fig. 3) or by curve fitting of the experimental polarization curve to the theoretical curve<sup>6,7</sup>.

(i) 3-parameter curve fitting ( $I_{\text{cor}}$ ,  $b_a$  and  $b_c$ )

The corrosion current may be obtained from experimental data  $I_{\text{exp}}(E_i)$  by minimising the least square criterium  $D_{\text{expth}}$

$$D_{\text{expth}} = \sum_i [I_{\text{exp}}(E_i) - I_{\text{th}}(E_i)]^2 \quad (4)$$

where  $i_{\text{th}}(E)$  is supposed to be given by

$$i_{\text{th}}(E) = I_{\text{cor}} \{ \exp [2.3 (E - E_c)/b_a] - \exp [-2.3 (E - E_c)/b_c] \} \quad (5)$$

The model  $I_{\text{th}}$  is a 3-parameter model :  $I_{\text{cor}}$ ,  $b_a$  and  $b_c$ . It is always possible to take 0.12 V for initial starting value of the Tafel slopes, it is then necessary to choose an initial starting value for the corrosion current.

<sup>6</sup> F. Mansfeld, Werkstoffe Korros. 28 (1977) 6.

<sup>7</sup> P. Hougaard and D. H. Britz, Corrosion Science, 23 (1983) 271.

(ii) 2-parameter curve fitting ( $b_a$  and  $b_c$ )

The corrosion current density  $I_{cor}$  is a linear parameter and  $b_a$  and  $b_c$  are non-linear parameters, so it is possible to eliminate  $I_{cor}$  in a nonlinear regression<sup>8,9,10</sup>. As a matter of fact differentiating  $D_{expth}$  (eq. 4) with respect to  $I_{cor}$  gives :

$$\partial D_{expth} / \partial I_{cor} = -2 \sum_i [I_{exp}(E_i) - I_{th}(E_i)] \partial I_{th}(E_i) / \partial I_{cor} = 0 \quad (6)$$

provided that  $D_{expth}$  is minimal. From eq. 6, linear in the parameter  $I_{cor}$ , one obtains

$$I_{cor} = \frac{\sum_i I_{exp}(E_i) \{ \exp [2.3 (E_i - E_{cor})/b_a] - \exp [-2.3 (E_i - E_{cor})/b_c] \}}{\sum_i \{ \exp [2.3 (E_i - E_{cor})/b_a] - \exp [-2.3 (E_i - E_{cor})/b_c] \}^2} \quad (7)$$

Substituting  $I_{cor}$  in eq. 5 using eq. 7 gives a reduced model. The reduced model is a non-linear model with only two unknown parameters  $b_a$  and  $b_c$ . The advantage of this new method is to reduce the dimension of the space of parametric search and to avoid the need of a starting value for  $I_{cor}$ . The method is not quicker with 2 parameters than with 3 as the calculation of the current (eq. 7) is now longer. Example of use of the method is given in the figure 4.

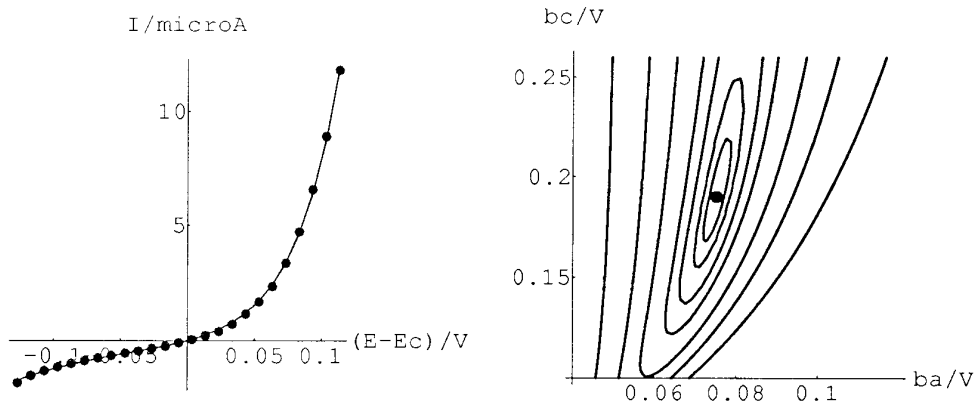


Figure 4 : Experimental data (points) and fitted curve (solid line) and isocriterion curve.  $I_{cor} = 0.37 \mu A$ ,  $b_a = 0.075 V$ ,  $b_c = 0.19 V$ .

Since the model now only depends on 2 parameters, it is possible to plot 2D isocriterion curves. Figure 4 shows that the parameter  $b_a$  is determined more precisely than  $b_c$ .

<sup>8</sup> Identification de modèles paramétriques à partir de données expérimentales, E. Walter et L. Pronzato, Masson, Paris, 1994.

<sup>9</sup> W. H. Lawton and E. A. Sylvestre, Technometrics, 13 (1971) 461.

<sup>10</sup> R. H. Barham and W. Drane, Technometrics, 14 (1972) 757.